

TABLE III. Values of experimental parameters for 2024-T351 aluminum.

Parameters	Low-velocity flying plates	High-velocity flying plates
Flyer plate velocity (cm/μsec)	0.125	0.33
Peak stress (Mbar)	0.110	0.345
Sound speed, <i>c</i> (cm/μsec) ^a	0.80±0.02	0.93±0.05
Sound speed, <i>c</i> (cm/μsec) ^b	0.81	...
<i>G</i> (Mbar)	0.54±0.07	0.59±0.25
<i>K</i> (Mbar)	1.27	2.28
$\sigma_e - \sigma_f$ (Mbar)	0.025	0.065
$Y_e + Y_f$ (Mbar)	0.013±0.008	0.025±0.008
Coordinate of point <i>M</i> , Fig. 2	5.5	4.5
Flyer plate thickness (cm)	0.32 (nominal)	0.32 (nominal)

^a Aluminum free-surface velocity vs depth measurements.

^b Immersed-foil water-gauge measurement.

Eq. (6)]. From Eq. (5) the elastic sound speed is

$$c^2 = d\sigma/d\rho = V(K + 4G/3) = FV, \quad (12)$$

where *F* is called the longitudinal elastic modulus and *V* is the specific volume. Experiments with flyer plates give values of both *c* and *V*, so that *F* may be calculated. The dependence of *F* on the stress can be determined if experimental data are available at two or more stress levels. Replacing *K* with $-VdP/dV$ there results

$$G = 3(F - K)/4 = 3(\rho c^2 + VdP/dV)/4. \quad (13)$$

The quantity dP/dV must first be approximated by $d\sigma_H/dV$ where σ_H is on the upper, or Hugoniot, curve of Fig. 6. Then the variables *G*, *F*, and *K* can be evaluated by using experimentally related values of *V* and *c*.

Equation (10) now becomes

$$\sigma_e - \sigma_f = (Y_e + Y_f)(K + \frac{4}{3}G)/2G, \quad (14)$$

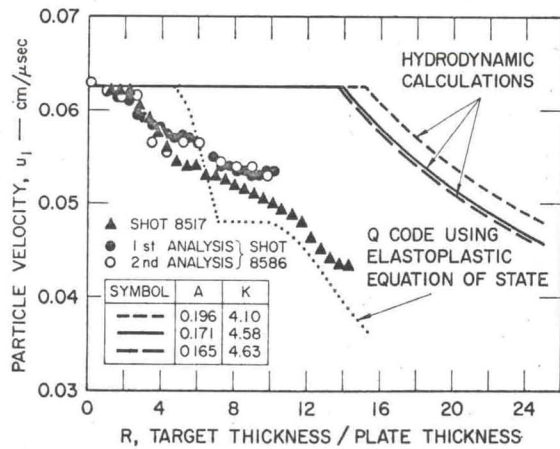


FIG. 9. Peak particle velocity in aluminum target hit by an aluminum projectile.

or by use of Eq. (12)

$$Y_e + Y_f = 1.5[1 - (K/\rho c^2)](\sigma_e - \sigma_f), \quad (15)$$

where *K* can be approximated as explained above. It was expected that the experiments which give *V* and *c* for an elastic wave would also give, at least approximately, values of $(\sigma_e - \sigma_f)$, so that the value of $(Y_e + Y_f)$ could be calculated. Once these values are known as, say, functions of the volume, Eq. (3) can be used to construct a tentative hydrostat, so that another approximation can be made for dP/dV , and the process of calculating *G* and $(Y_e + Y_f)$ can be repeated. Because the experiments fail to show a definite separation

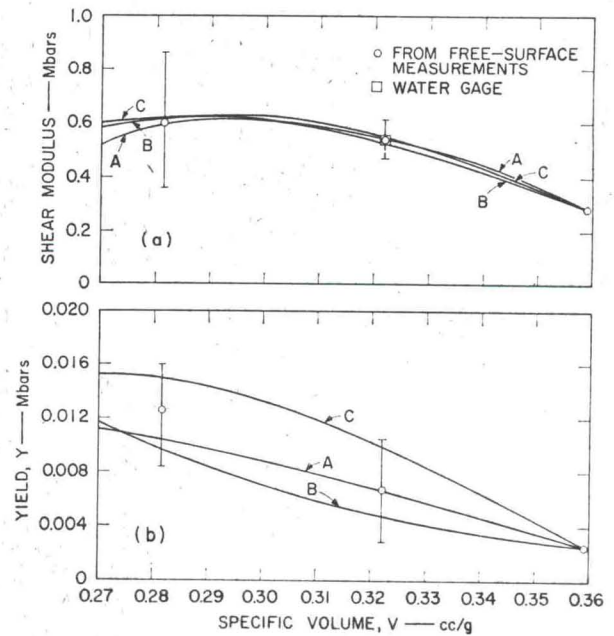


FIG. 10. Shear modulus *G* and yield stress *Y* vs specific volume *V*.

profiles of stress
aluminum projectile
aluminum target
thickness 0.322
velocity 0.125

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at intervals
parameters
the elasto-
the elastic
pressure wave
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ss-strain

Fluid
model

0.0
0.0
2.785
0.765
1.66
0.428